

# WP9 - Numerical capability development for liquid icing conditions



AIRBUS SAS  
BOMB  
CIRA  
CU  
DASSAV  
ONERA – O. Rouzaud  
POLIMI  
POLYMO  
SAFRAN  
TUBS  
TUDA  
TUS

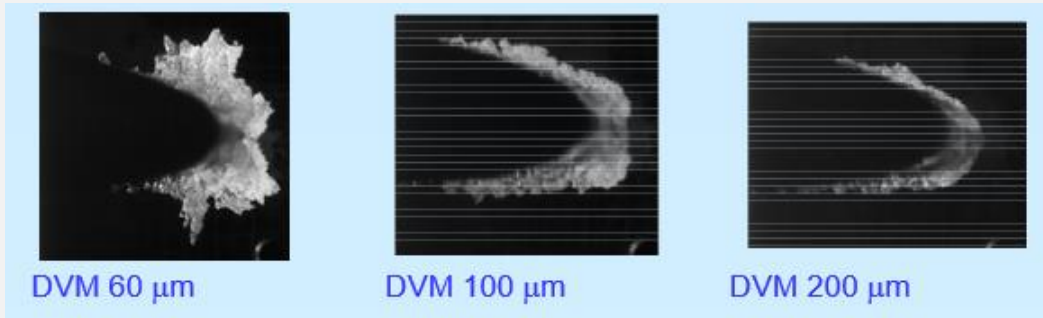
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# Context

Objectives: **improve and validate current 2D/3D numerical tools** with respect to **Appendix C** and **Appendix O** conditions, so that they can be used for both design and certification of aircraft, rotorcraft and engines

Why is it so important to work on SLDs?

- Because large droplets do not behave as smaller droplets: more inertial, more energetic, ...
- Need for adapted or specific physical models



Why is it so important to work on the numerical tools?

- To improve the overall performances of the industrial solvers in 3D
- To improve the solution by itself

\* Appendix C is associated to clouds / “small” cloud droplets

\* Appendix O is associated to Freezing Drizzle and Freezing Rain conditions / Supercooled Large Droplets (SLD)

ICE GENESIS Public Workshop - 3<sup>rd</sup> November 2022

# Work plan



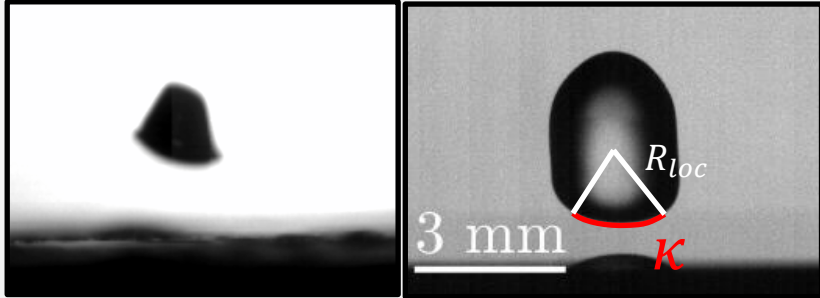
## Decomposition into 4 Tasks

- Task 9.1: Basic experiments to provide missing data for model development
  - Task 9.2: Model improvements and implementation in 2D tools for calibration and preliminary validation
    - Phenomena under consideration: drop impact, ice roughness, ~~liquid film runback~~
    - More or less academic experiments performed in different labs (CU, ONERA, TUDA, TUBS)
    - Improvement or development of new physical models (CIRA, ONERA, POLIMI, TUBS, TUDA, TUS)
- +
- Task 9.4: Improvement of 3D ice accretion numerical methodologies (CIRA, ONERA, POLIMI, POLYMO)
    - Working on numerical models for meshing (automatic meshing, remeshing) for 3D test cases
- ||
- Task 9.3: Model integration in 3D numerical tools and preliminary validation
    - Combining physical models and numerical methods to answer Ice Genesis WP9 objectives
    - Towards the industrial configurations of WP11

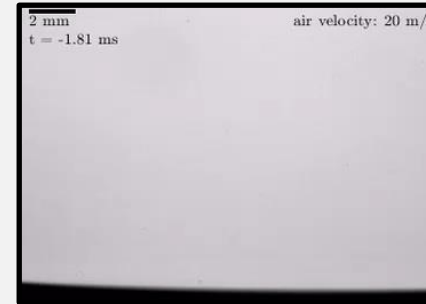
# Drop Impact – Experimental activities



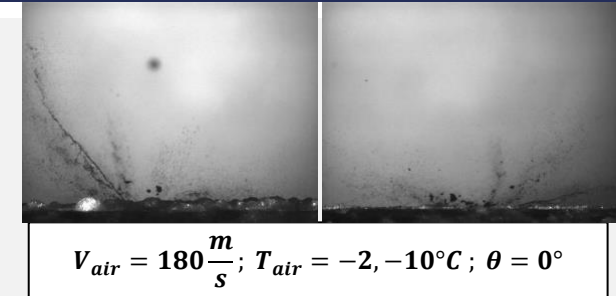
Drop impact implies to characterize...



1 - Drop deformation



2 - Impact regime



$$V_{air} = 180 \frac{m}{s}; T_{air} = -2, -10^{\circ}C; \theta = 0^{\circ}$$

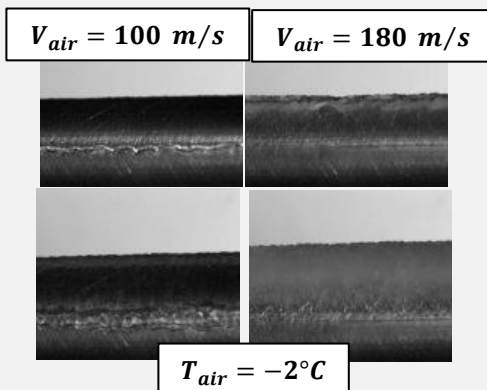


3 - Mass deposition

Melting drop

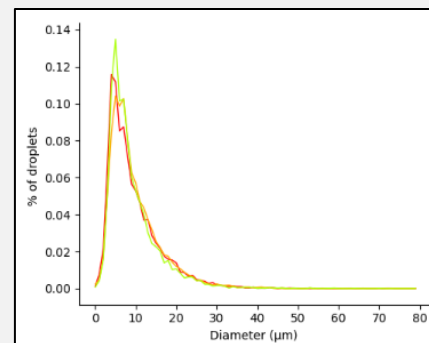


5 - Ice Accretion

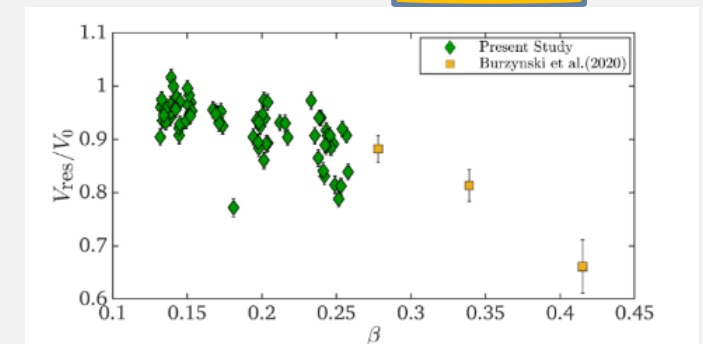


$T_{air} = -2^{\circ}C$

4 - Secondary droplets



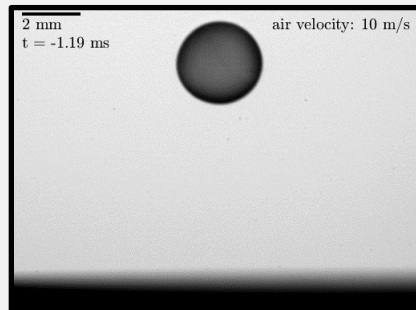
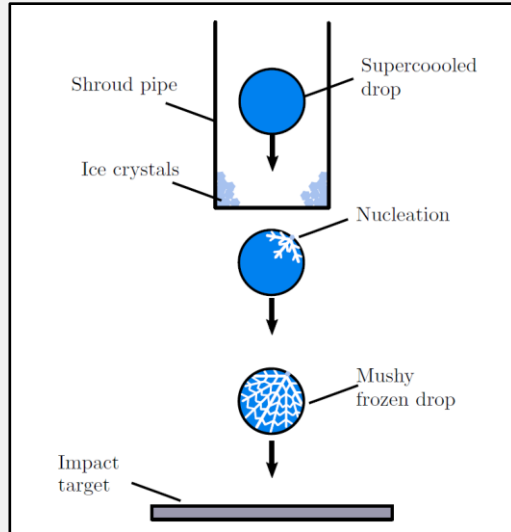
Temperature influence (5, -10, -20)  
 $V_{air} = 100 \text{ m/s}$



# Drop Impact – Experimental activities



And also new or unexpected phenomena

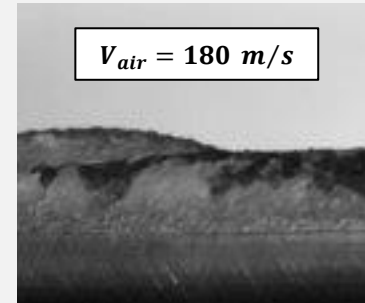


Dendritically frozen drop impact

$T_{air} = -10^{\circ}\text{C}$



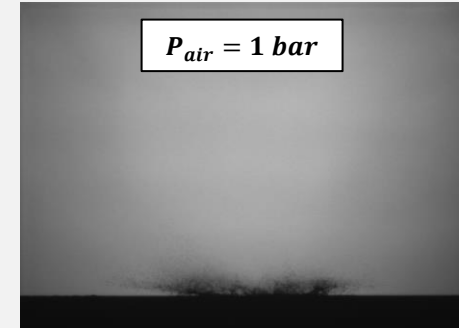
$V_{air} = 180 \text{ m/s}$



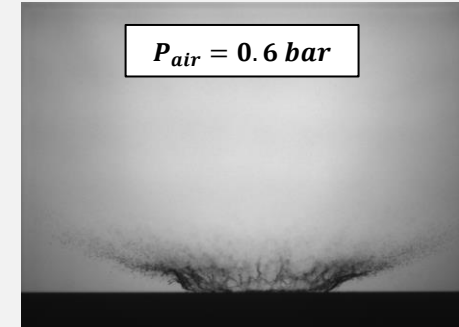
Erosion phenomenon

$D_0 \approx 325 \mu\text{m}$  ;  $V_{air} = 140 \text{ m/s}$  ;  $T_{air} = 15^{\circ}\text{C}$

$P_{air} = 1 \text{ bar}$



$P_{air} = 0.6 \text{ bar}$



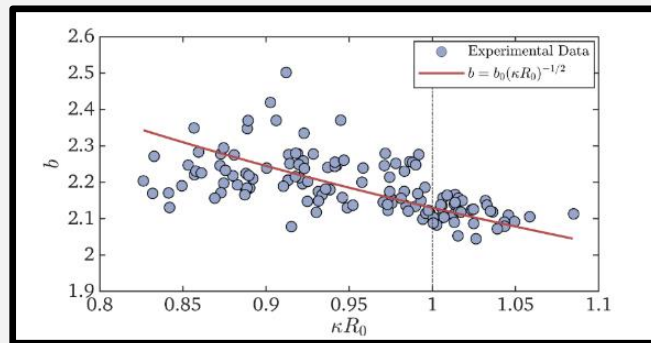
Altitude effect

# Drop Impact – Physical modelling



From very detailed models...

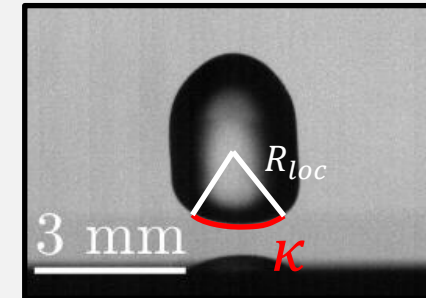
- Droplet deformation prior to the impact
  - Spherical droplet:  $r/R_o = b \sqrt{t U_o/R_o} \Rightarrow r^+ = b \sqrt{t^+}$
  - Analysis of the IG data provides:  $b = b_o/\sqrt{\kappa R_o}$ ,  $b_o = 2.12$



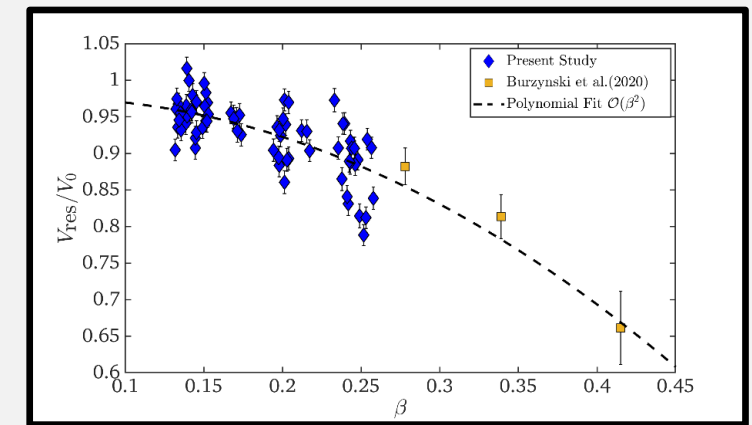
Curvature influence

⇒ influence on the splashing parameter  $\beta$  (Riboux-Gordillo model)

- Mass deposition
  - Depending on the splashing parameter  $\beta$
  - Flight conditions may exceed  $\beta > 0.4$  (what happens above 0.45?)
- Liquid film runback (not presented here)



$r$  radius of the wetted area  
 $R_o$  radius of the impinging drop  
 $U_o$  drop velocity



Residual volume on the surface

# Drop Impact – Physical modelling

To applied ones used in the industrial solvers

- Droplet deformation => how to define the radius of curvature  $\kappa$ ?
- Mass deposition
  - Adaptation of the Trontin-Villedieu and the Wright models on the impact function
  - Application to an accretion experimental test case (Ice Genesis database)
- Secondary droplets
  - Approach based on Riboux-Gordillo and Burzinsky-Bansmer-Roisman models
  - Description of the spray by a log-normal law defined by parameters estimated from RG

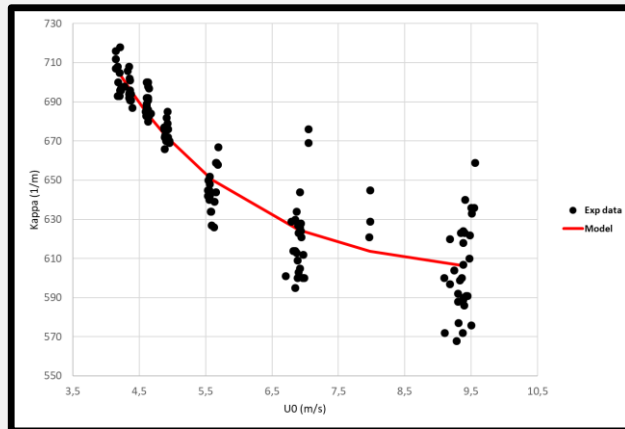
$$\kappa(U_0) = C_0 * [C_1 + C_2 \tanh(C_3 U_0)]$$

$$\kappa = \min(\kappa(U_0), 715)$$

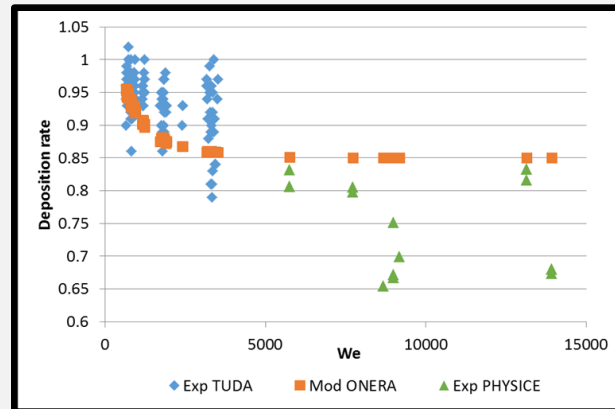
$$\text{ONERA model: } f(\tilde{\kappa}_n) = 1 - C_1 \frac{\tilde{\kappa}_n^2}{C_2 + \tilde{\kappa}_n^2}$$

Wright model:

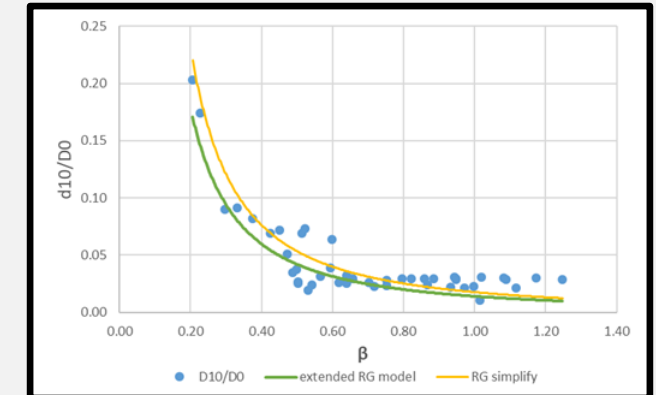
$$f_m = \frac{m_s}{m_0} = C_3 [1 - \sin(\theta_0)] [1 - e^{-0.0092(K_{L,n} - 200)}]$$



Droplet deformation



Mass deposition



Mean diameter vs. splashing parameter

# Experimental activities – Ice Roughness

Objective: investigate influence of icing conditions on the characteristics of ice accretion roughness

Experiments performed in TUBS Icing Wind Tunnel

- HMDI airfoil: Span=0.5m, Chord=0.7m, non-symmetrical airfoil based on NASA CRM
- Operating conditions encompassing both App.C and App. O

$V_{air} = 40 \text{ m/s}$  ;  $AoA = 0^\circ$  ;  $T_\infty = -5 \text{ to } -16^\circ\text{C}$  ; *Reynolds number*  $Re \approx 2e6$

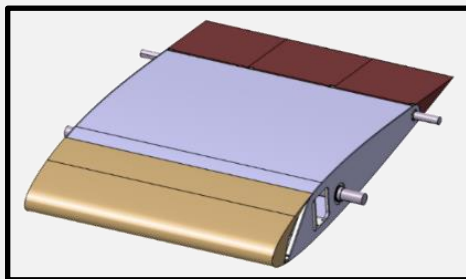
$MVD_\infty \approx 19\mu\text{m}$  (App. C) &  $70\mu\text{m}$  (App. O) ;  $LWC_\infty \approx 0.88\text{g/m}^3$  (App. C) &  $0.56\text{g/m}^3$  (App. O)

Accretion time  $t = 1.5, 3, 6, 9 \text{ min}$

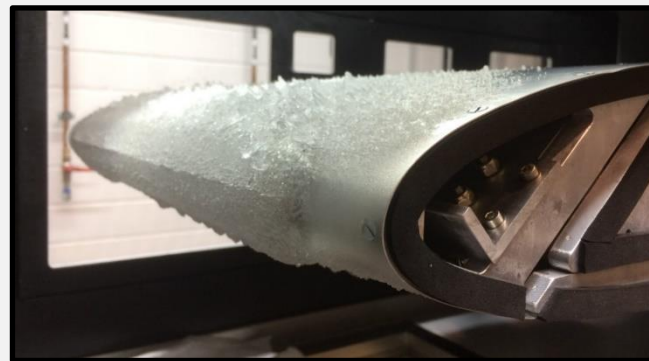
Experiments include several levels of  $\eta_{f,0}$

Combinations of  $\eta_{f,0}$  and  $A_c$  not investigated before

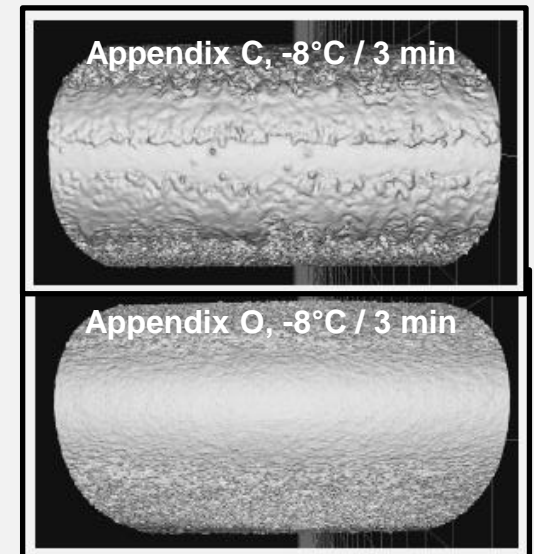
Insight on effects of non-symmetric airfoils



Airfoil sketch



Iced airfoil in the test section



Accreted ice  
Front view

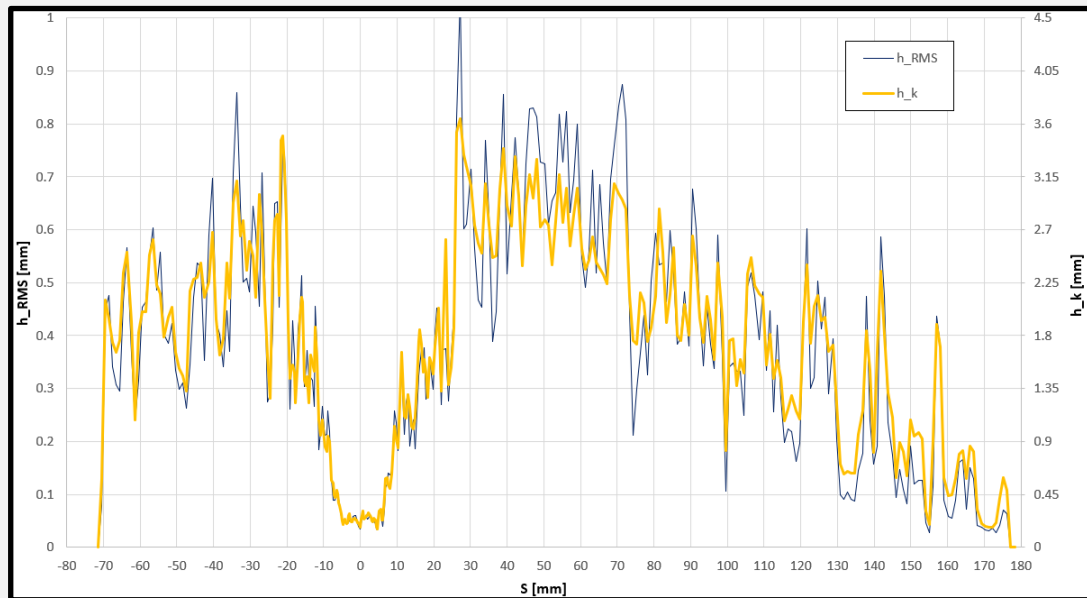


# Ice Roughness – Experimental activities

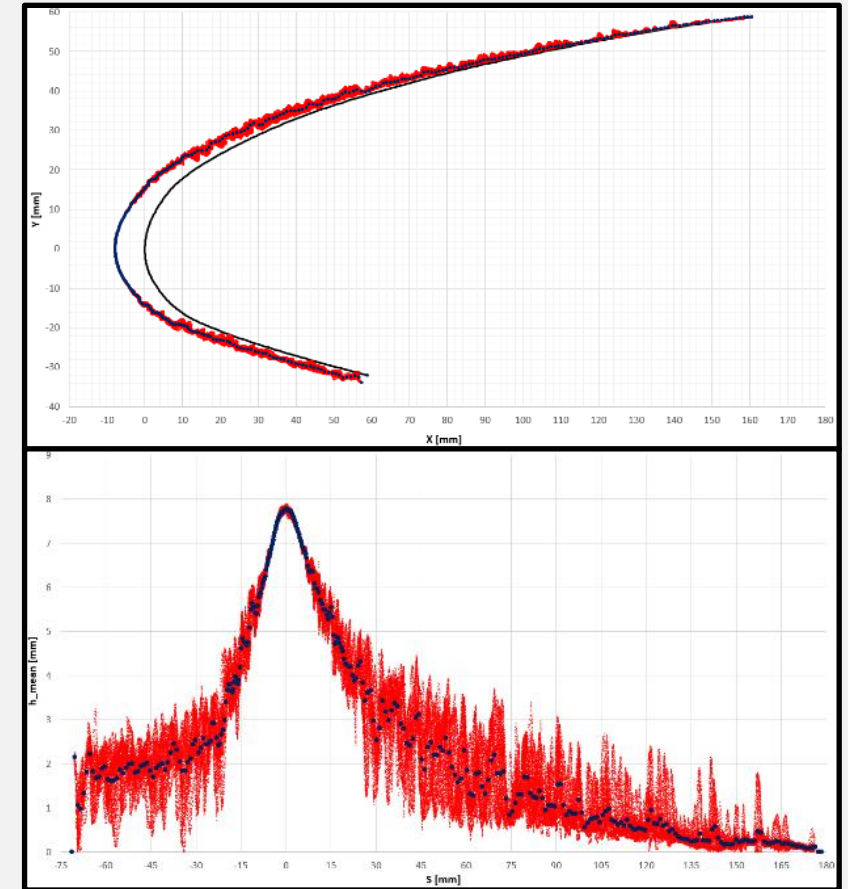


## How to analyse the ice roughness?

- Digitalization of the ice shape (photogrammetry method)
- Development of tools for statistical analysis
- **Post-processing of the experimental data**
- Assessment of the tools



$h_k$  (orange) and  $h_{RMS}$  (blue) vs. curvilinear abscissa



Top view: clean and iced airfoil

Bottom view:  $h_{mean}$  (slices in red, mean in black dot)

# Ice Roughness – Experimental activities

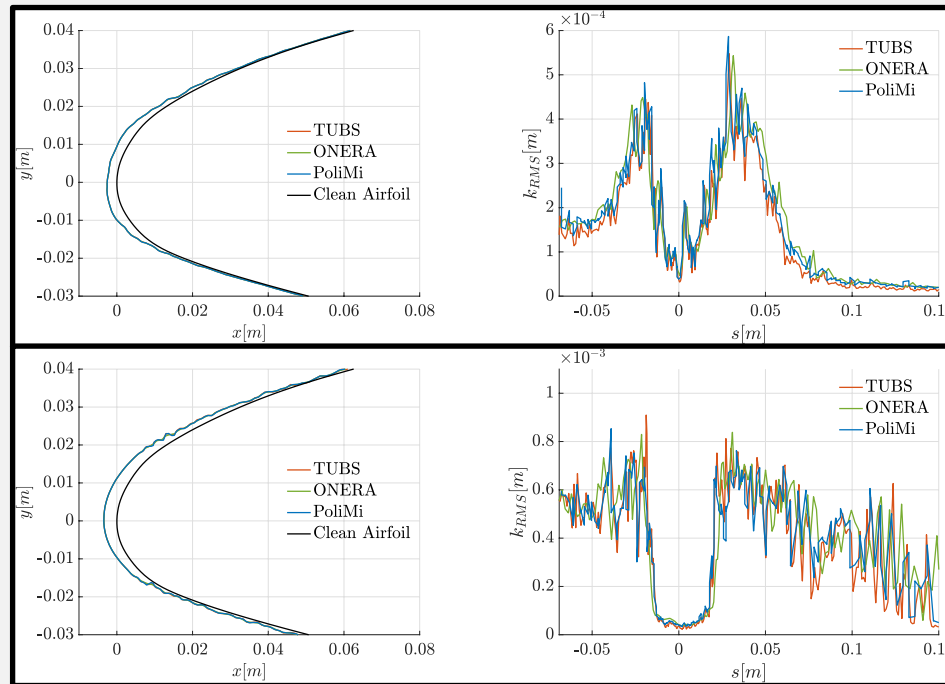


## How to analyse the ice roughness?

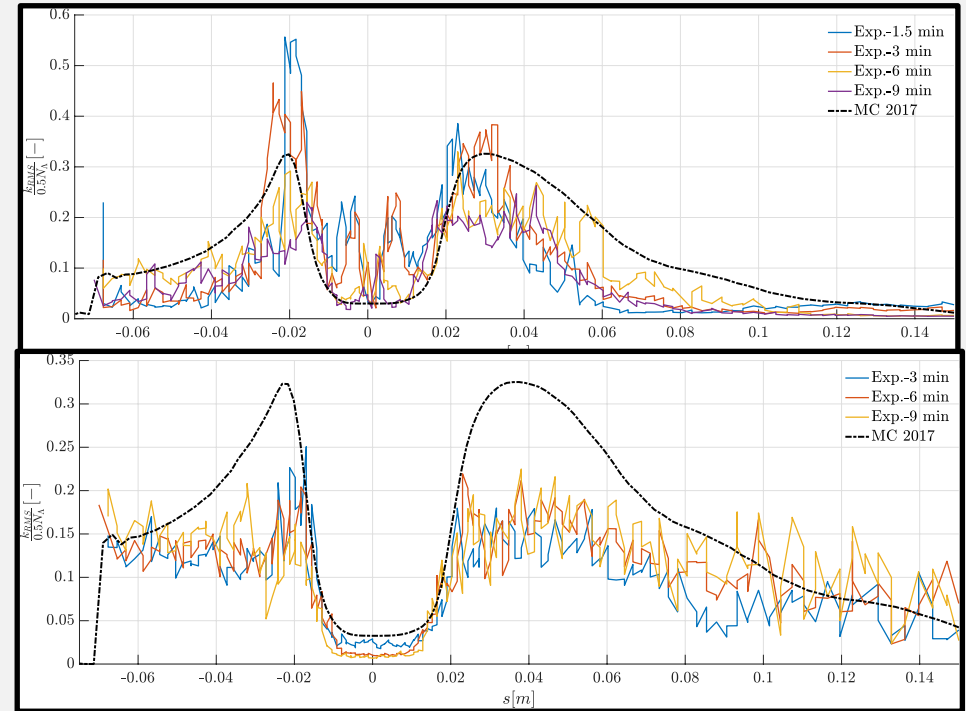
- Digitalization of the ice shape (photogrammetry method)
- Development of tools for statistical analysis
- Post-processing of the experimental data
- **Assessment of the tools**

App. C

$T = -12^{\circ}\text{C}$  ;  $t = 3 \text{ min}$



Ice shape (left) /  $k_{\text{RMS}}$  (right)



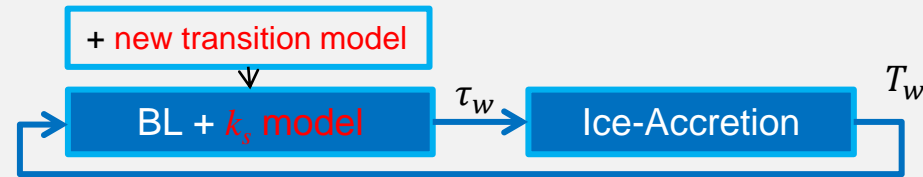
Rq comparison with McClain's model

$T = -8^{\circ}\text{C}$  / Top view App.C / Bottom view App.O

# Ice Roughness – Physical modelling



Model based on Fortin's bead model (roughness height) and Abu-Gahnnam & Shaw model (transition)



- Roughness height model

$$\text{Bead size: } e_b = \alpha_0 L Re_\tau^{\alpha_1} We_\tau^{\alpha_2} H_1(\theta, \Delta\theta) H_2(Re_b)$$

$$k_s = \alpha_3 e_b$$

- Transition model

$$\gamma = 1 - e^{-\beta_1 \eta^{\beta_2}}$$

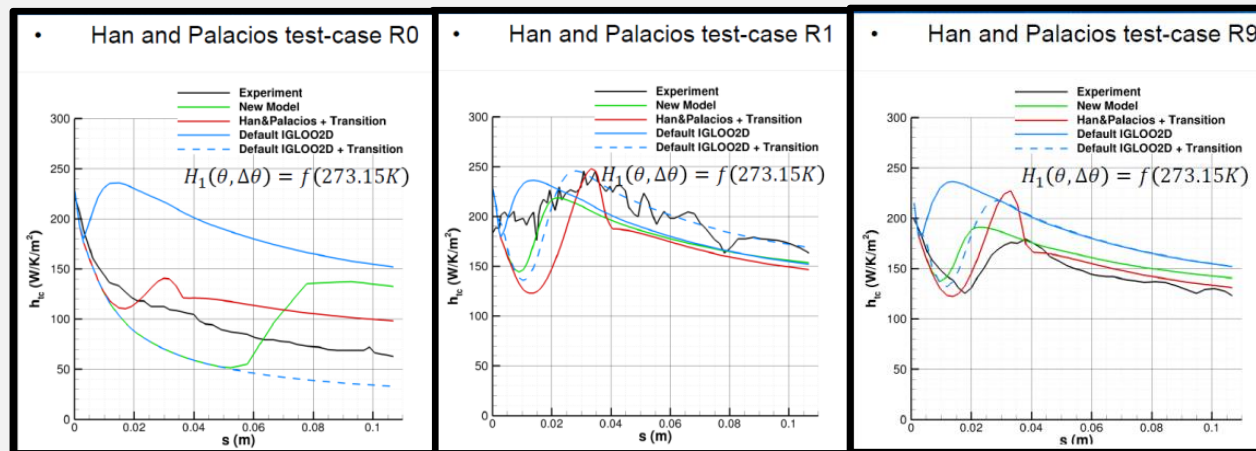
- Optimization process to determine the best values  $\alpha_3$  of and  $\eta$  using an IA approach  
Performed on 3 of the Han & Palacio's Heat Transfer Coefficient (htc) database

# Physical modelling – Ice Roughness



Assessment of the model based on

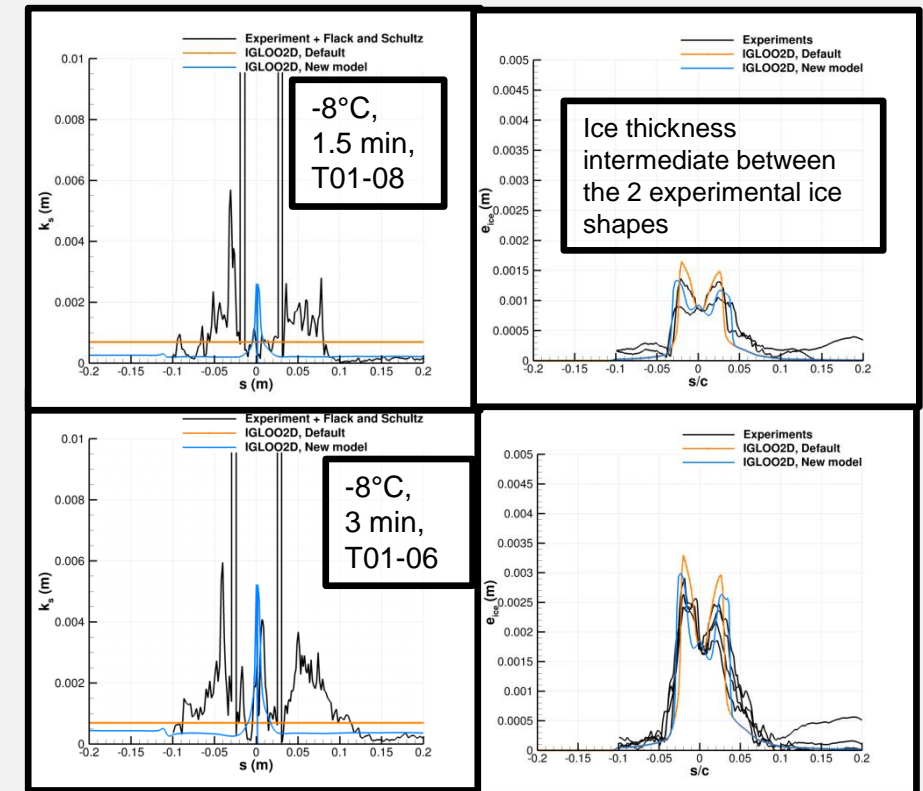
- Roughness height characteristics (TUBS database)
- Impact of the roughness height on measured data (htc - Han & Palacio's database, ice shape - TUBS database)



Heat transfer coefficient comparisons



Good agreement for most of the cases



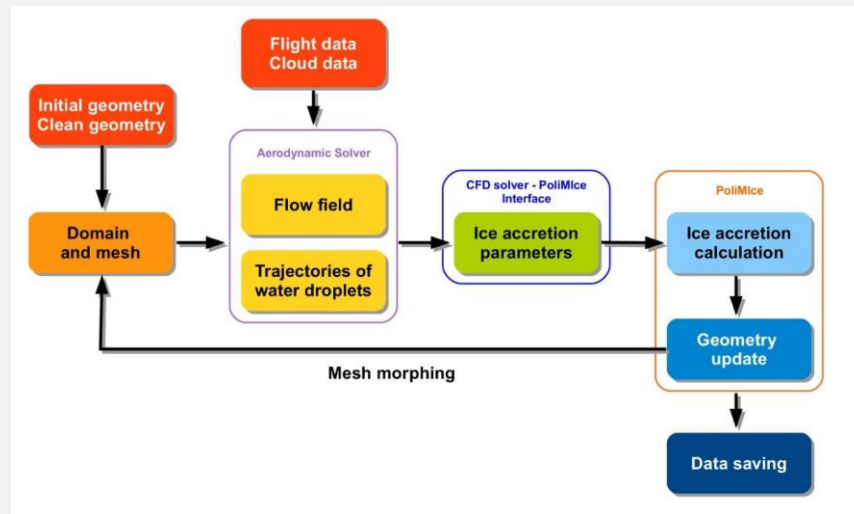
Roughness height (left) / Ice thickness (right) comparisons

# Numerical methods - Introduction

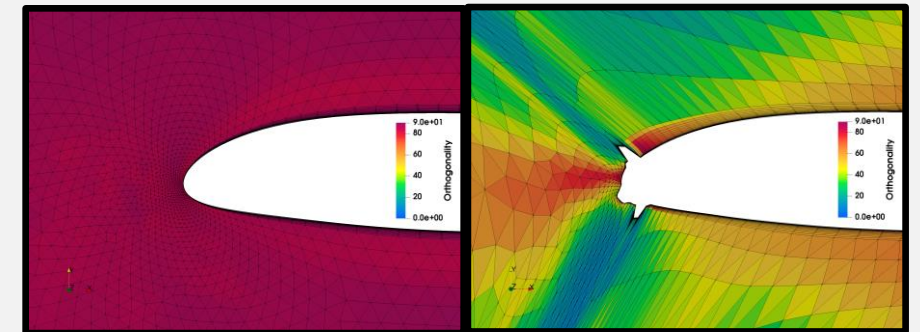
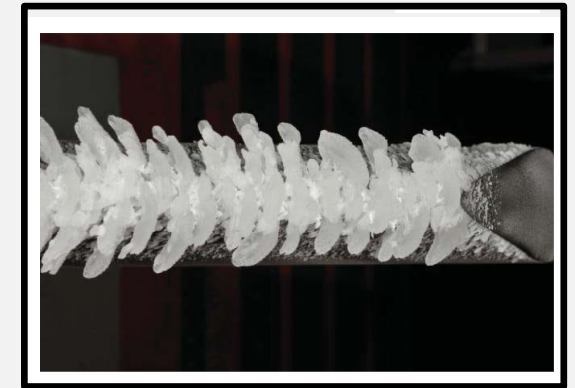


Objective: develop efficient numerical methods to handle 3D simulations

- Aiming at **Predictor-Corrector or MultiStep approaches**
- Considering mesh adaptation to account for ice surface growth



3D ice shape



Mesh displacement

- But
  - On physical grounds, 3D ice shape can be quite complex, 3D ice  $\neq$  2D ice
  - On numerical/modelling grounds, need to deal with mesh displacement, ice density modelling, mass conservation, ...

# Numerical methods - Results

Several candidate methods have been developed by the partners:

- 3D Multi-step Immersed Boundary Method, Lagrangian displacement of surface mesh for ice accretion only (CIRA)
- 3D Predictor-Corrector plus remeshing, with Lagrangian displacement (ONERA)
- 3D Multi-step on conformal meshes with level-set and remeshing (POLIMI)
- 3D Multi-step on conformal meshes with Lagrangian (POLYMO)
- Very preliminary approaches for mass conservation are available

Definition of Numerical benchmark tests for T9.4

- Baseline calculation: NACA23012 2D extruded cases (Ice Prediction Workshop database)

| Run      | V [m/s] | T [C]  | P [Pa] | MVD [ $\mu$ m] | LWC [g/m <sup>3</sup> ] | AoA [°] | Time [s] | Remarks       |
|----------|---------|--------|--------|----------------|-------------------------|---------|----------|---------------|
| Case 241 | 103     | -23°   | 92528  | 30             | 0.42                    | 2°      | 300      | Rime ice      |
| Case 251 | 103     | -12.6° | 91700  | 21.5           | 1.64                    | 2°      | 400      | Monomodal SLD |
| Case 252 | 103     | -12.6° | 91700  | 21.5           | 1.64                    | 2°      | 400      | Bimodal SLD   |

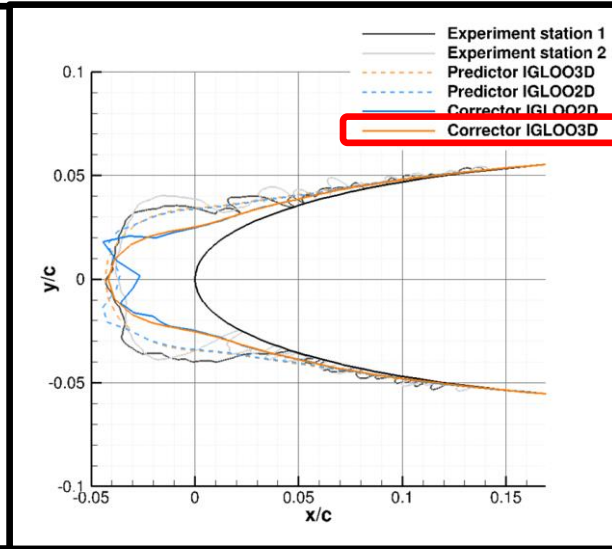
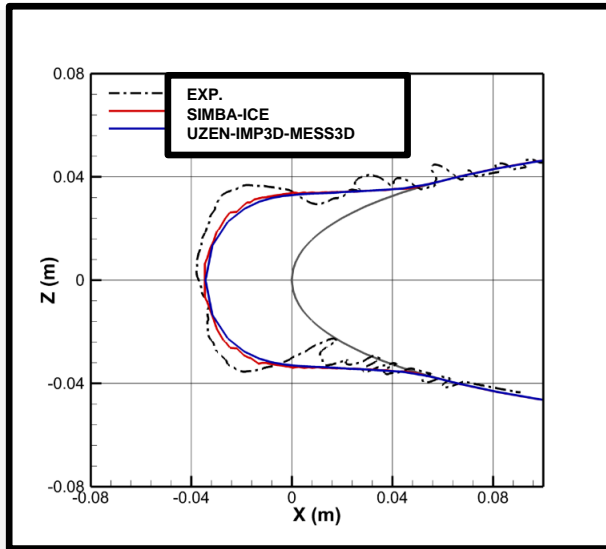
- **Benchmark tests: 30° swept NACA0012 (Ice Prediction Workshop database)**

|          |     |      |       |      |     |    |      |           |
|----------|-----|------|-------|------|-----|----|------|-----------|
| Case 361 | 103 | -16° | 92321 | 34.7 | 0.5 | 0° | 1200 | Rime ice  |
| Case 362 | 103 | -7°  | 92321 | 34.7 | 0.5 | 0° | 1200 | Glaze ice |



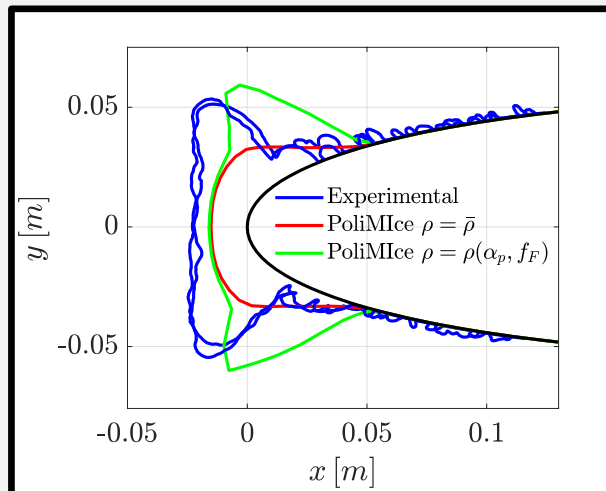


# Numerical methods – Results



## Case 361 – Rime ice (CIRA, ONERA)

- Correctly captured in 3D

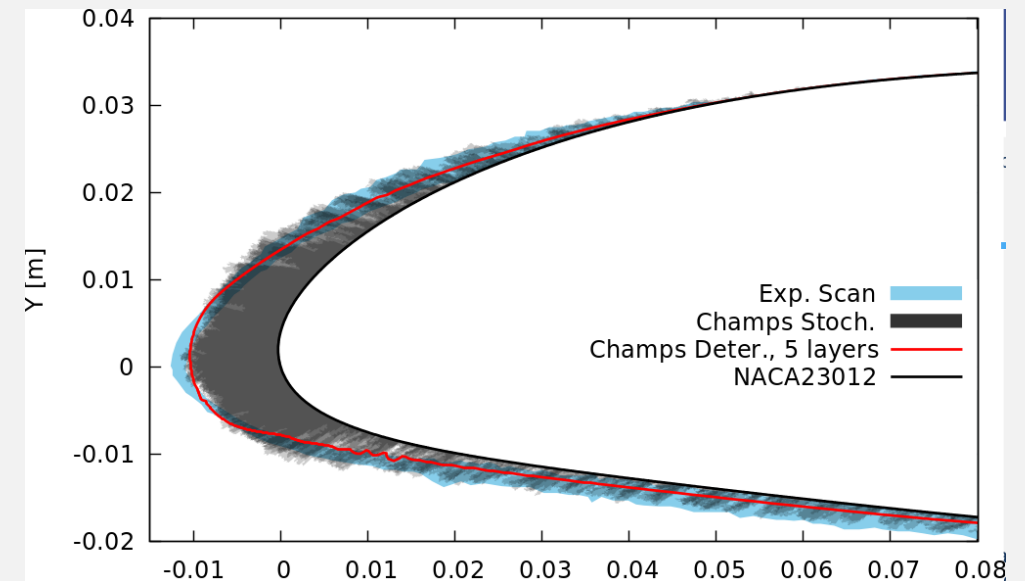


## Case 362 – Glaze ice (POLIMI)

- Less correctly captured in 3D
- Ice density plays a role

## Case 241 – Rime ice (POLYMO)

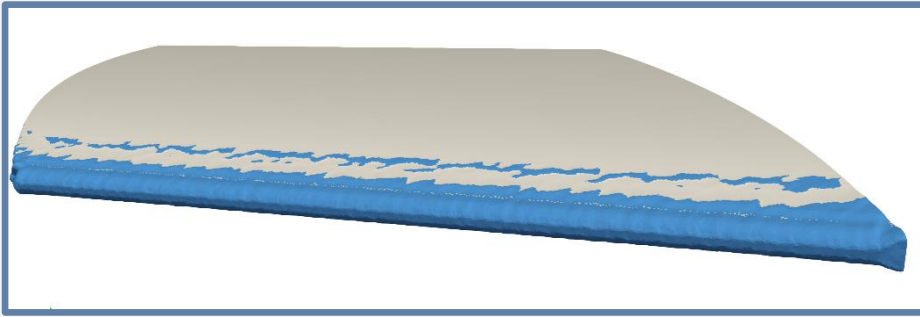
- Stochastic approach vs. Deterministic approach



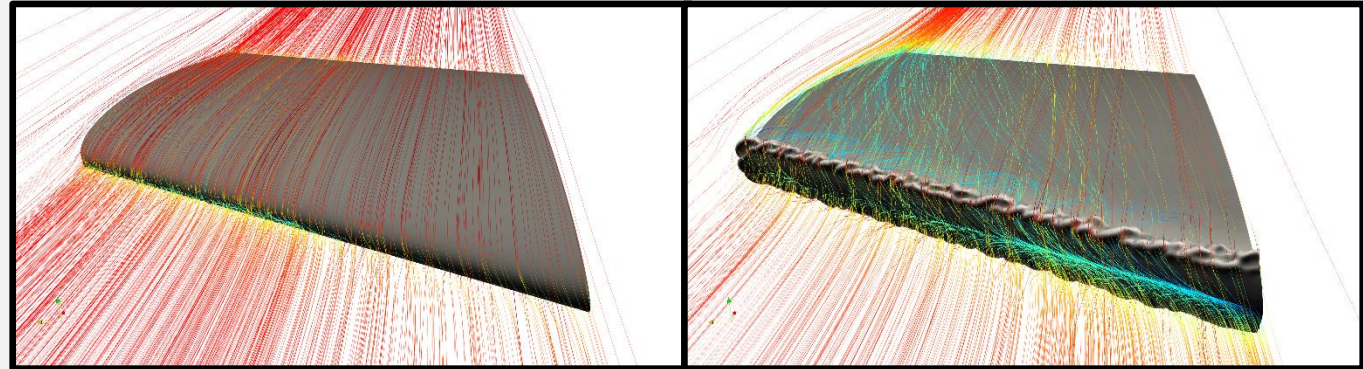
# Numerical methods – Some more results

## Observations

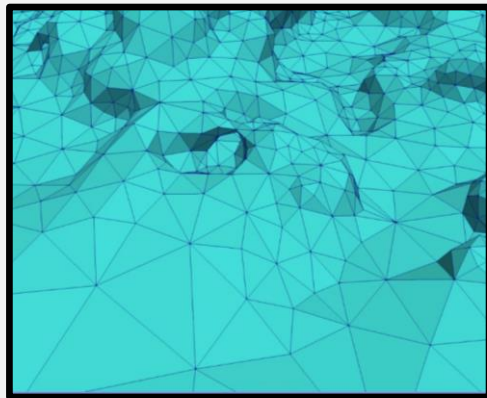
- Physics of 3D ice accretion results in non-negligible numerical difficulties
- Unsteady ice accretion is important to describe the whole process
- Models are still not satisfactory (e.g. ice density)



Multi-connected ice shapes (ice in blue)



Collection efficiency coefficient: single step (left), multistep (right)



Mesh issues with very refined grid leading very small ice structures



# Conclusions & Perspectives



## Main achievements on the experimental and modelling parts so far

- Academic experiments performed on two important topics for SLD: drop impact and roughness
- Roughness
  - Experimental methodology clearly defined
  - Ongoing activity to build a model to account for roughness & transition
- Drop impact
  - Insights gained thanks to some experiments or some complex/basic models but...
  - Improvements of the existing models are not that conclusive
- New phenomena to be possibly investigated (Dendritically Frozen Drop, erosion, drop deformation)
- High-altitude effects to be investigated



## Main achievements on the numerical part so far

- Extension of the capabilities of the 3D tools ongoing (Predictor-Corrector, Multistep)



# THANK YOU



This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 824310. This text reflects only the author's views and the Commission is not liable for any use that may be made of the information contained therein.

